

COST BENEFIT ANALYSIS OF A TWO UNIT COLD STANDBY SYSTEM WITH CORRELATED FAILURES AND REPAIRS AND INSPECTION TIME

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ABSTRACT: *This paper presents the analysis of a two - unit cold standby system with inspection time. There are two repairmen i.e. expert and assistant repairman. The failure and repair times of each unit have been assumed to be correlated and their joint density has taken as a bivariate exponential. Using the regenerative point technique, various reliability characteristics of interest have been obtained. The behavior of MSTF has been also studied graphically.*

KEYWORDS: *Mean time to system failure (MTSF), Inspection time, Regenerative point technique, Cold standby system, Availability Analysis.*

INTRODUCTION

Several authors including references [1-3] and [6-8] in the field of reliability theory have analyzed two unit-cold standby systems assuming that there is only single repair facility to repair a failed unit. As soon as an operative unit fails, its repair starts instantaneously by a repairman. This assumptions not hold in many real-life systems. Sometimes it has been observed that system manager has two repairmen i.e. expert and assistant repairman. As soon as operative unit fails, the expert repairman instructs to the assistant repairman what tools and equipments are needed to repair the failed unit. After inspection of the failed unit, assistant repairman starts the repair of the failed unit. In all the above systems [1-5], it has been assumed that failure and repair times are uncorrelated. But, in practical life, it has been also observed that there are some systems [6-8] with correlated failure and repair time.

Keeping these facts in view, we have analyzed here a two-unit cold standby system with correlated failure and repair time and inspection time.

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MODEL DESCRIPTION

The system consists of two identical units. Initially one unit is operative and the other is cold standby. Upon failure of operative unit, the standby unit is put into operation instantaneously and the expert repairman instructs to the assistant repairman what tools and equipments are needed to repair the failed unit. After inspection, the failed unit is taken up for repair by assistant repairman. A repaired unit works like a new one. The system fails completely if during inspection time and during the repair of a failed unit, the other unit also fails. When failed unit is under inspection or under repair, the other failed unit waits for inspection. The inspection time distribution is negative exponential with parameter θ . The joint distribution of failure (X) and repair (Y) times of each unit is bivariate exponential with respective parameters (α, β) .

NOTATION AND STATES

In order to define the states of the system, we define the following symbols,

N_0/N_s :unit is in normal mode and operative / standby.

$FI/FwI/FI_c$: failed unit is under inspection/waits for inspection/ inspection is continued from earlier state.

Fr/Frc : failed unit is under repair/ repair continued from earlier state.

With these symbols, the possible states of the system are as follows:

UP States: $\underline{S}_0=(N_0, N_s)$, $\underline{S}_1=(FI, N_0)$ $\underline{S}_2=(Fr, N_0)$

Failed States: $S_3=(Frc, FwI)$, $S_4=(FI_c, FwI)$ $\underline{S}_5=(Fr, FwI)$

The underlined states are regenerative states. A transition diagram of the system model is shown in Fig 1.

TRANSITION PROBABILITIES AND SOJOURN TIMES

We obtain the following non-zero elements of the transition probability matrix P:

$$p_{01} = 1, p_{12} = \theta / [\theta + \alpha (1 - r)], p_{15}^{(4)} = \alpha (1 - r) / [\theta + \alpha (1 - r)],$$

$$p_{20} = \beta / [\alpha + \beta], p_{21}^{(3)} = \alpha / [\alpha + \beta] \text{ and } p_{51} = 1$$

Clearly, the above probabilities satisfy the following relations:

$$p_{01} = 1, p_{12} + p_{15}^{(4)} = 1, p_{20} + p_{21}^{(3)} = 1 \text{ and } p_{51} = 1$$

The mean sojourn times in various states are:

$$T_0 = 1/\alpha(1 - r), T_1 = 1/[\theta + \alpha(1 - r)], T_2 = 1/[(\alpha + \beta)(1 - r)],$$

$$T_3 = T_5 = 1/\beta(1 - r), T_4 = 1/[\theta]$$

MEAN TIME TO SYSTEM FAILURE

Considering the failed states S_3, S_4 and S_5 as absorbing, we have by simple probabilistic reasoning, the following recurrence relations:

$$\pi_0(t) = Q_{01}(t) \pi_1(t) \tag{1}$$

$$\pi_1(t) = Q_{12}(t) \pi_2(t) + Q_{14}(t) \tag{2}$$

$$\pi_2(t) = Q_{20}(t) \pi_0(t) + Q_{23}(t) \tag{3}$$

Taking the Laplace-Stieltjes transform of (1)- (3) and using the well known formula for MTSF, we get

$$\text{MTSF} = (T_0 + T_1 + p_{12}T_2) / (1 - p_{12}p_{20}) \tag{4}$$

AVAILABILITY ANALYSIS

From the arguments used in the theory of regenerative processes, we observe:

$$A_0(t) = M_0(t) + q_{01}(t) \odot A_1(t) \tag{5}$$

$$A_1(t) = M_1(t) + q_{12}(t) \odot A_2(t) + q_{15}^{(4)}(t) \odot A_5(t) \tag{6}$$

$$A_2(t) = M_2(t) + q_{20}(t) \odot A_0(t) + q_{21}^{(3)}(t) \odot A_1(t) \tag{7}$$

$$A_5(t) = q_{51}(t) \odot A_1(t) \tag{8}$$

Where,

$$M_0(t) = \exp[-\alpha(1 - r)t], M_1(t) = \exp[-\{\theta + \alpha(1 - r)\}t]$$

$$\text{And } M_2(t) = \exp[-(\alpha + \beta)(1 - r)t]$$

By taking the laplace transform of (5)-(9), we can obtain $A_0^*(s)$, Using this result, the steady-state availability of the system is

$$A_0 = \lim_{t \rightarrow \infty} A_0(t) = \lim_{s \rightarrow 0} sA_0^*(s) = \frac{N_1}{D} \quad (9)$$

Where,

$$N_1 = (T_0(1 - p_{12}p_{21}^{(3)} - p_{16}^{(4)}) + (T_1 + p_{12}T_2) \text{ and}$$

$$D = T_0p_{12}p_{20} + (T_1 + p_{15}T_4) + (T_2 + p_{23}T_3) + T_5p_{15}^4$$

BUSY PERIOD ANALYSIS

Using the definition of $B_i(t)$ and simple probabilistic reasoning, we have the following recursive relations:

$$B_0(t) = q_{01}t \odot B_1(t) \quad (10)$$

$$B_1(t) = W_1(t) + q_{12}(t) \odot B_2(t) + q_{15}^{(4)}(t) \odot B_5(t) \quad (11)$$

$$B_2(t) = W_2(t) + q_{20}(t) \odot B_0(t) + q_{21}^{(3)}(t) \odot B_1(t) \quad (12)$$

$$B_5(t) = W_5(t) + q_{51}(t) \odot B_1(t) \quad (13)$$

Where $W_1(t) = \exp[-\{\theta + \alpha(1 - r_1)\}t]$ $W_2(t) = \exp[-\{(\alpha + \beta)(1 - r)\}t]$

And $W_5(t) = \exp[-\{\beta(1 - r)t\}]$

By taking Laplace transform of (10) – (13), we can obtain $B_0^*(s)$. The steady state probability that both repairman are busy given by:

$$B_0 = \lim_{t \rightarrow \infty} B_0(t) = \lim_{s \rightarrow 0} sB_0^*(s) = \frac{N_2}{D} \quad (14)$$

Where, $N_2 = (T_1 + p_{12}T_2)$

COST ANALYSIS

1. The expected up-time of the system and busy period of repairman in (0, t) are:

$$\mu_{up}(t) = \int_0^t A_0(u) du$$

$$\mu_b(s) = \int_0^t B_0(u) du$$

So that

$$\mu_{up}^* (s) = \frac{A_0^* (s)}{s}$$
$$\mu_b^* (s) = \frac{B_0^* (s)}{s}$$

Now expected profit incurred in (0,t) is

$$P(t) = c_1 \mu_{up}(t) - c_2 \mu_b(t) \quad (15)$$

Where C_1 is the revenue per unit up time by the system and C_2 is the repair cost per unit time. Therefore the expected profit per unit time in steady state is

$$P = \lim_{t \rightarrow \infty} \frac{P(t)}{t} = \lim_{s \rightarrow 0} s^2 P_0^* (s) = C_1 A_0 - C_2 B_0 \quad (16)$$

CONCLUSION

To observe the effect of correlation (r) and inspection rate(θ) on the system performance, We plot the MTSF against correlation and inspection rate keeping the other parameters fixed. The curves are shown in figure 2. From these curve we observe the MTSF increases with increasing in correlation (r) and decreases with increasing in inspection rate (θ). Thus to obtain a high MTSF, we must have a high correlation and small inspection rate (θ). Hence we conclude that the system leads to a better overall performance for large value of correlation and small value of inspection rate.

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Transition Diagram

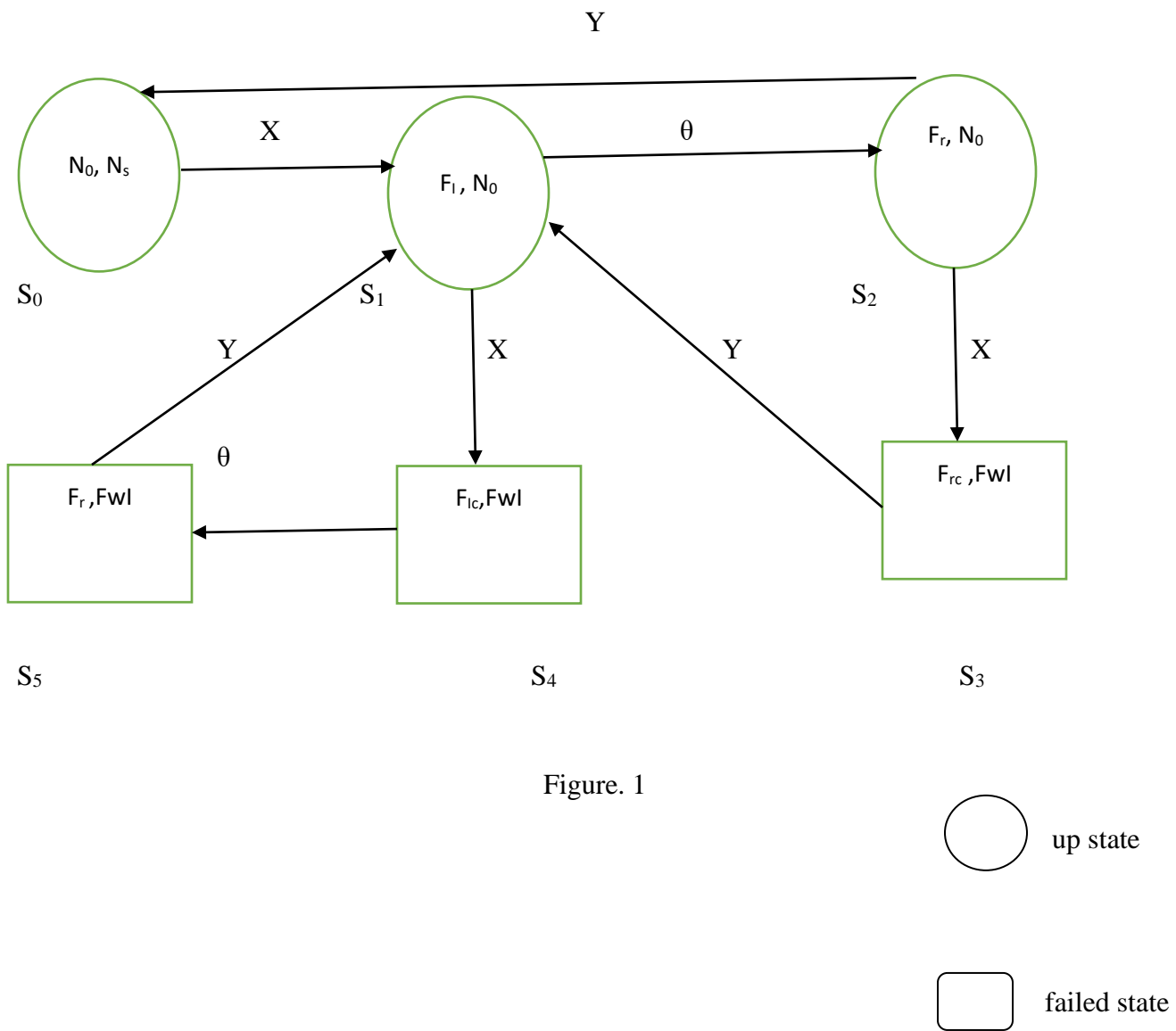


Figure. 1

Behaviour of MTSF w.r.t. to θ for different Values of r .

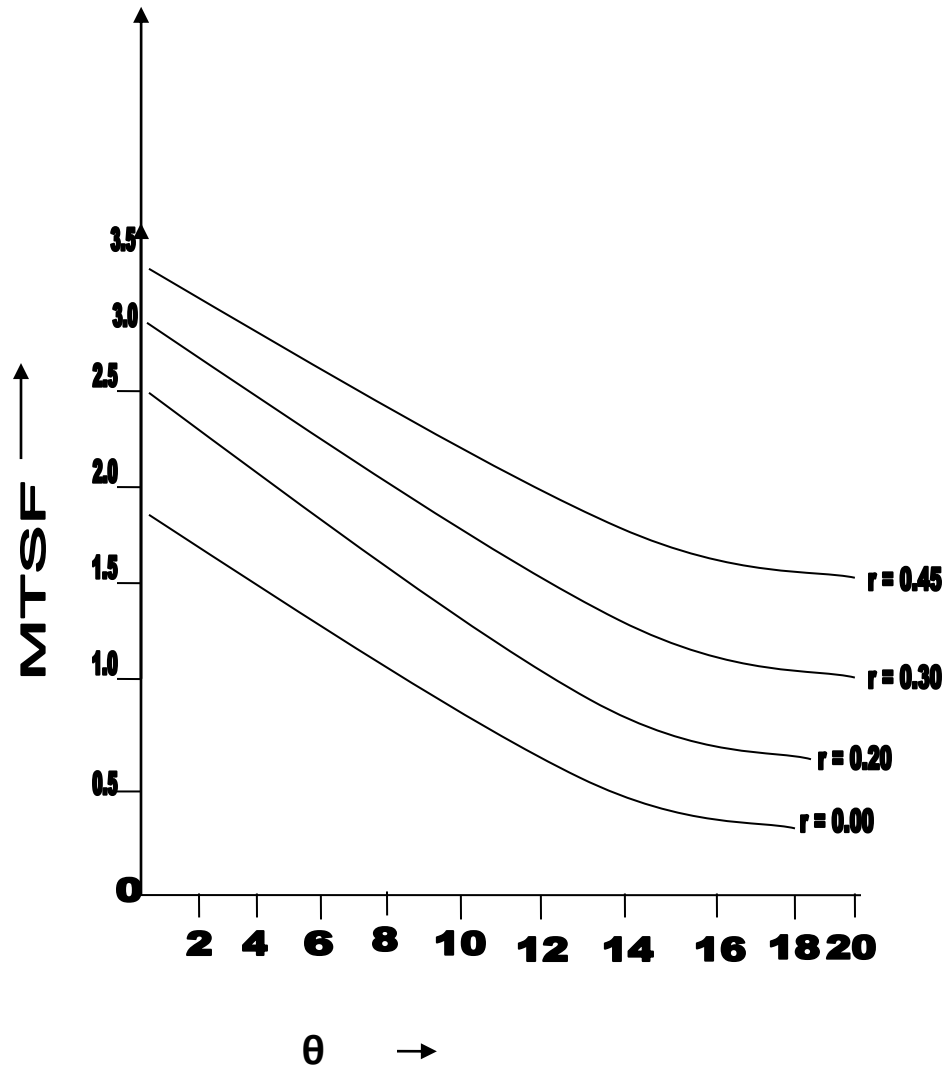


Figure 2